

Richtek **A**dvanced **C**onstant **O**n **T**ime Buck converters:

Richtek ACOT™ RT7275GQW EVM kit



Roland van Roy
FAE Richtek Europe

August 2014

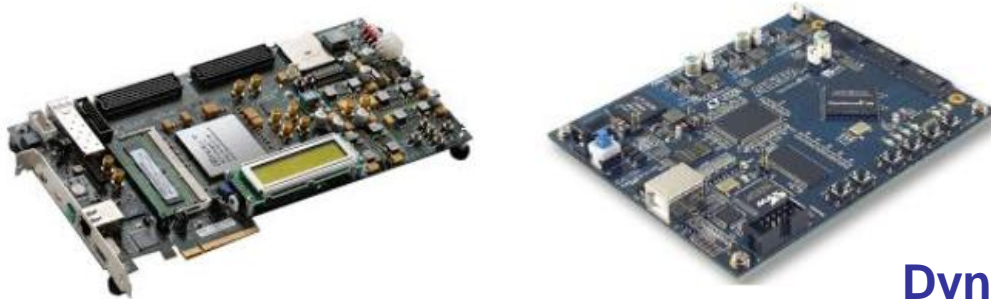
RICHTEK
your power partner.

Content

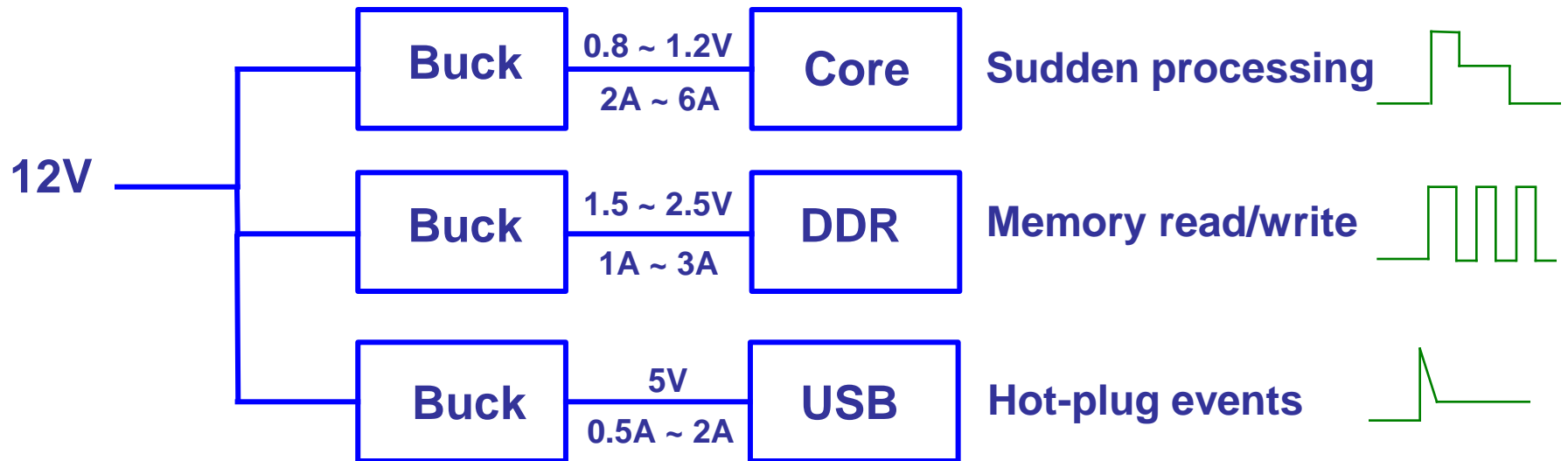
- ❑ Challenges with high load transient applications
- ❑ Current Mode buck converter versus ACOT
- ❑ ACOT design considerations
- ❑ RT7275GQW EVM kit parameters
- ❑ ACOT Frequently Asked Questions (FAQ)
- ❑ ACOT design tools & application notes

Challenges in powering High Transient Loads

FPGA, DSP and SoC applications can exhibit fast changing loads:

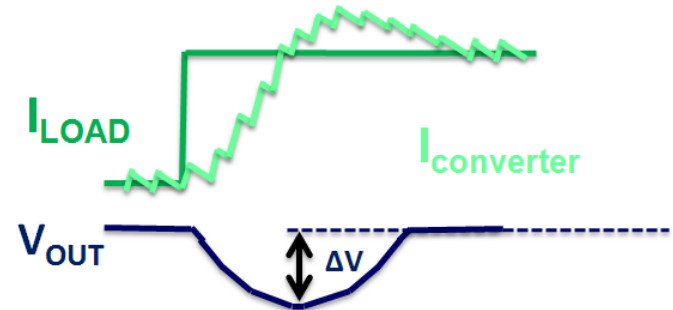
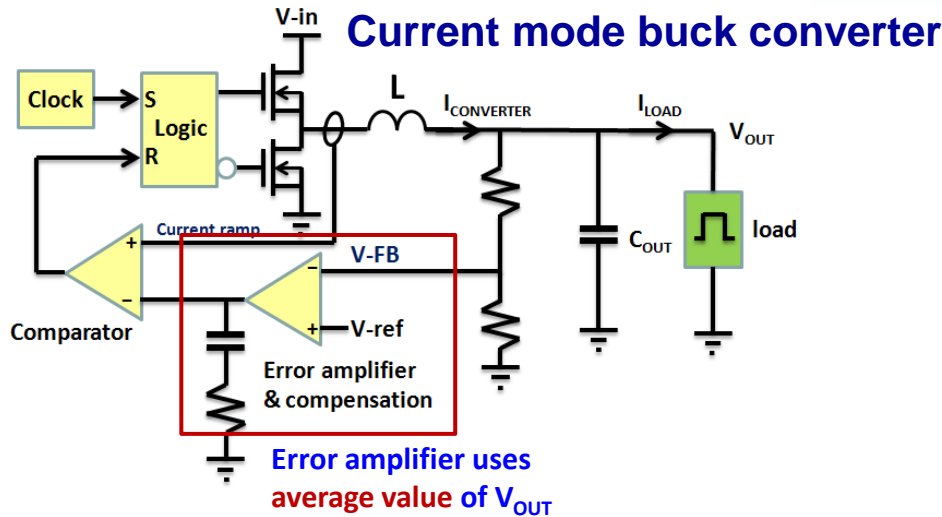


Dynamic load condition:

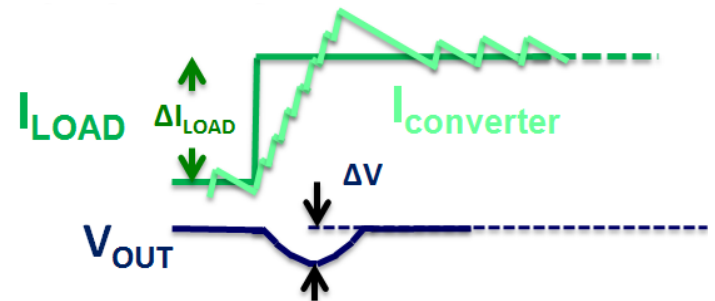
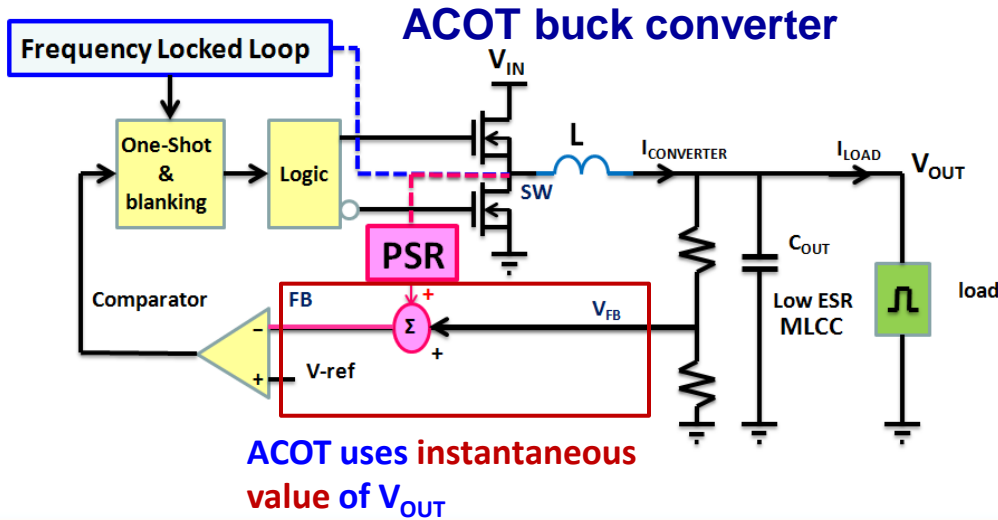


→ Output Voltage Sag under transient load should not affect normal operation

Current mode vs. ACOT buck converter reaction speed



Current mode buck takes several switch cycles to react on load transient.
Needs larger C_{OUT} for small ΔV



ACOT reaction speed is almost instantly.
 C_{OUT} can be smaller for same ΔV

Design considerations for ACOT Buck converters

Add low ESR C_{IN} for input rail filtering and check C_{IN} RMS current rating

Select L-value for 20 ~ 50% current ripple

EN for power sequence or connect to V_{IN} for auto-start.

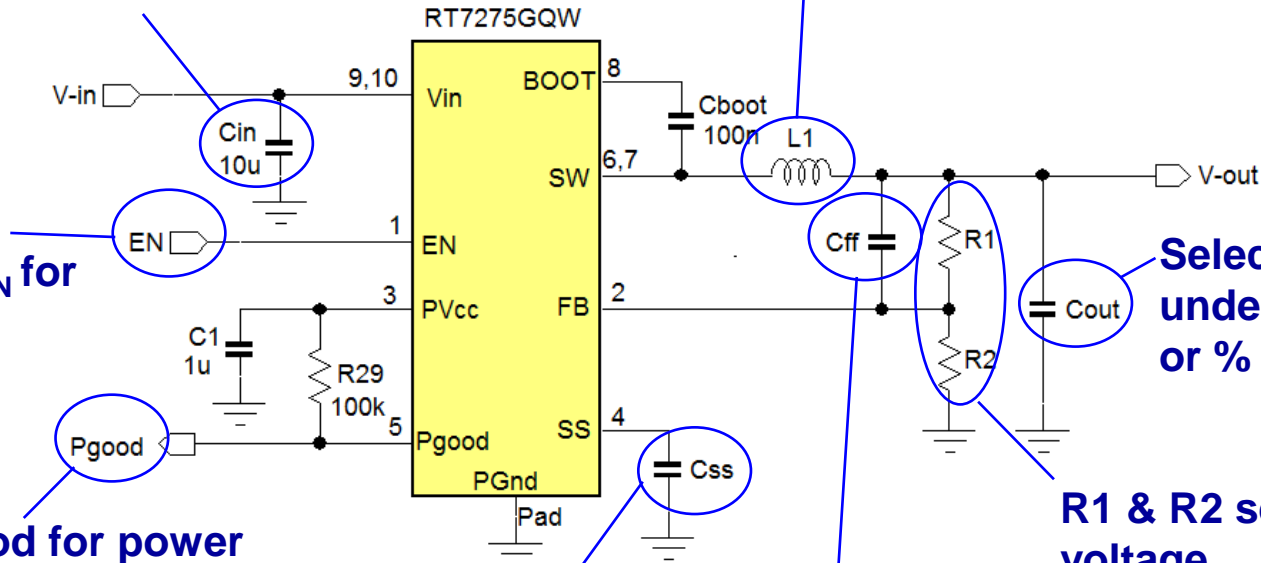
Select C_{OUT} for % sag under load transient or % output ripple

Pgood for power sequence or SoC enable

C_{SS} sets soft-start time

Add some C_{ff} for extra damping (high V_{OUT} and high C_{OUT} applications)

R1 & R2 set output voltage



RT7275GQW EVM KIT:

C_{IN} for $30mV_{pp}$ input ripple

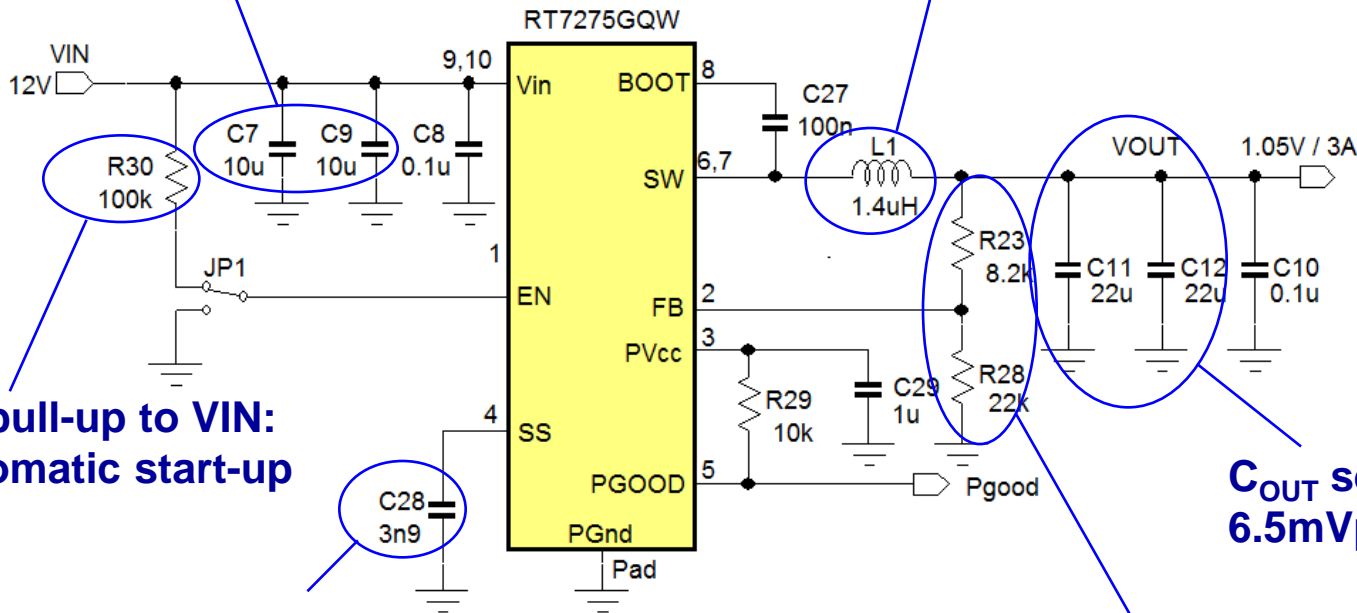
$L1 = 1.4\mu H$: Ripple = 1A (33% ripple)

EN pull-up to VIN:
Automatic start-up

$C_{SS} = 3.9nF$:
 $T_{SS} = 2.6msec$

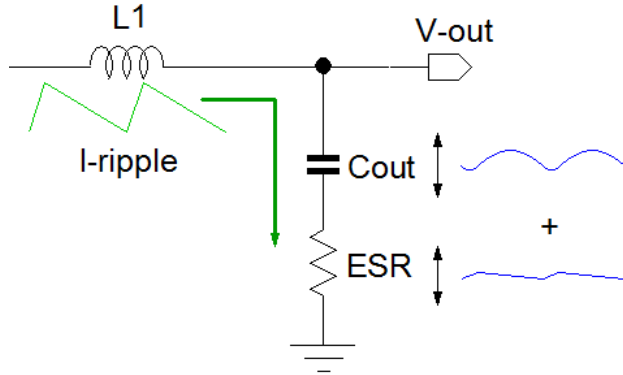
C_{OUT} selected for
 $6.5mV_{pp}$ output ripple

R1 & R2 set for 1.05V
output voltage
(C_{ff} is not needed for
this 1.05V application)



ACOT FAQ: Calculate and measure output ripple

How does output ripple happen?



Calculation method:

$$V_{RIPPLE} = V_{RIPPLE(ESR)} + V_{RIPPLE(C)}$$

$$V_{RIPPLE(ESR)} = \Delta I_L \times R_{ESR}$$

$$V_{RIPPLE(C)} = \frac{\Delta I_L}{8 \times C_{OUT} \times f_{SW}}$$

In the RT7275GQW 1.05V evaluation board:

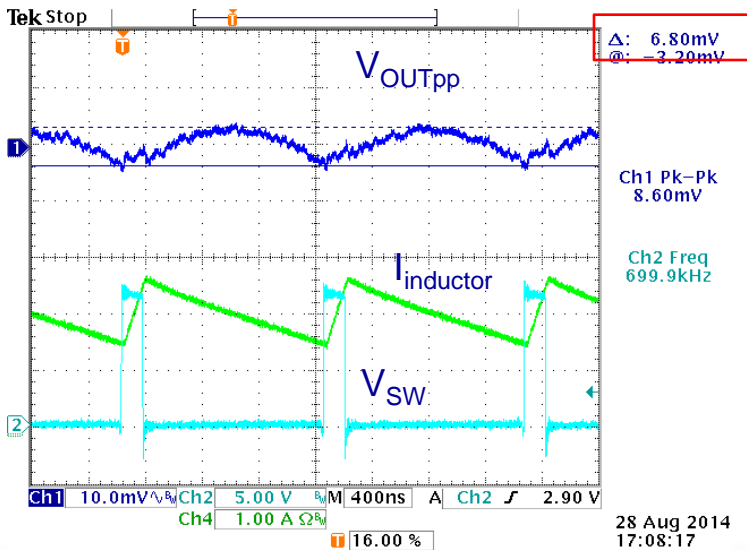
$$V_{RIPPLE(ESR)} = 1A \times 2.5m\Omega = 2.5mV$$

$$V_{RIPPLE(C)} = \frac{1A}{8 \times 44\mu F \times 0.7MHz} = 4mV$$

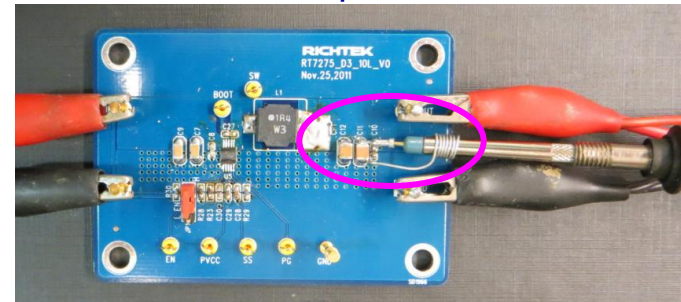
$$V_{RIPPLE} = 2.5mV + 4mV = 6.5mV$$

V_{RIPPLE} measured: 6.8mVpp

EVM measurement result



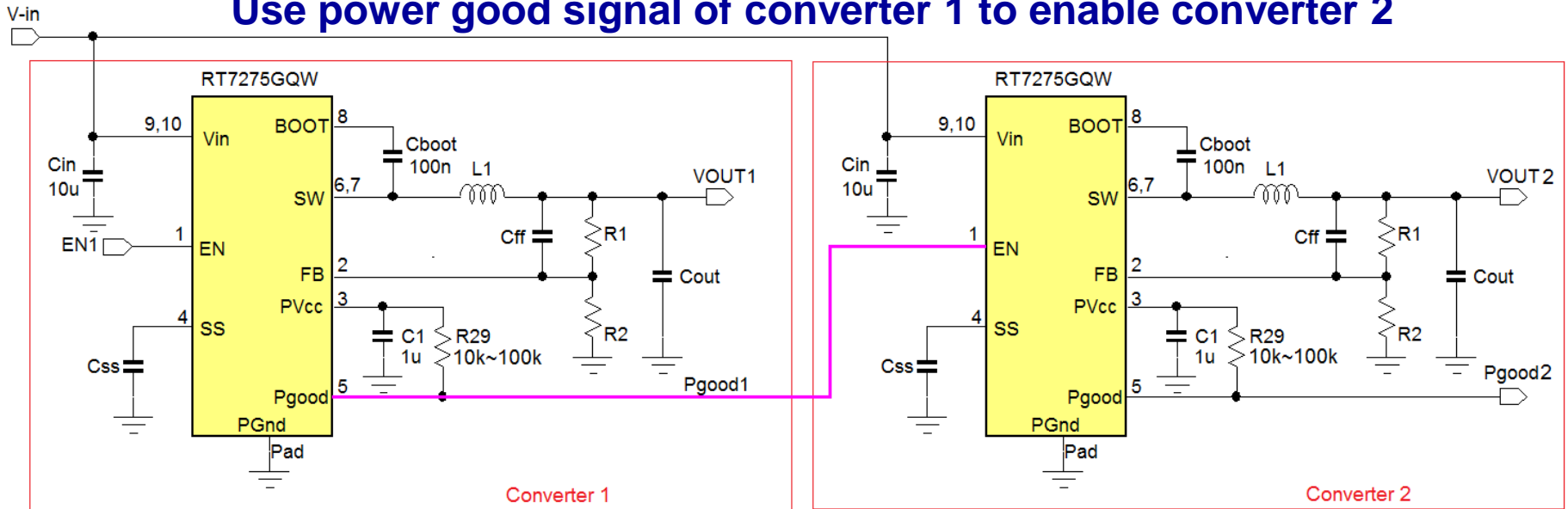
Measurement setup:



Use short probe leads to minimize inductor stray field noise pick-up

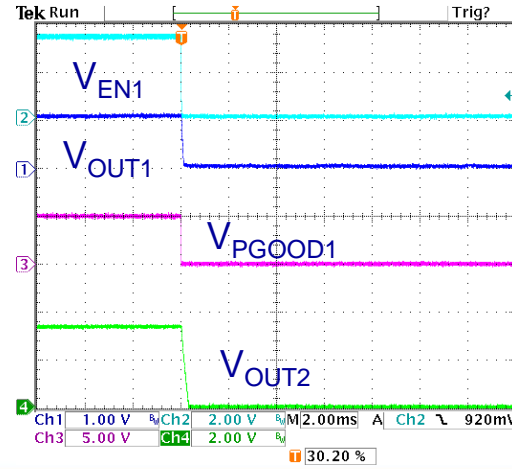
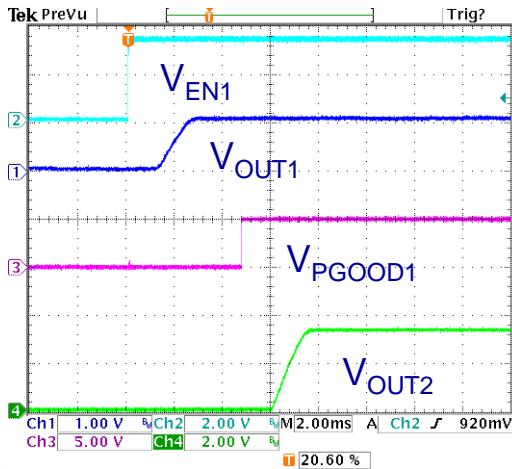
ACOT FAQ: How to make power sequence

Use power good signal of converter 1 to enable converter 2



Converter 1

Converter 2

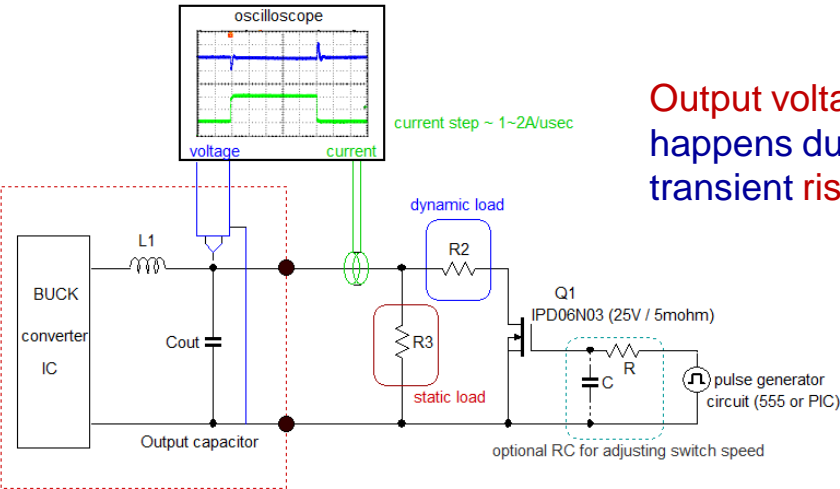
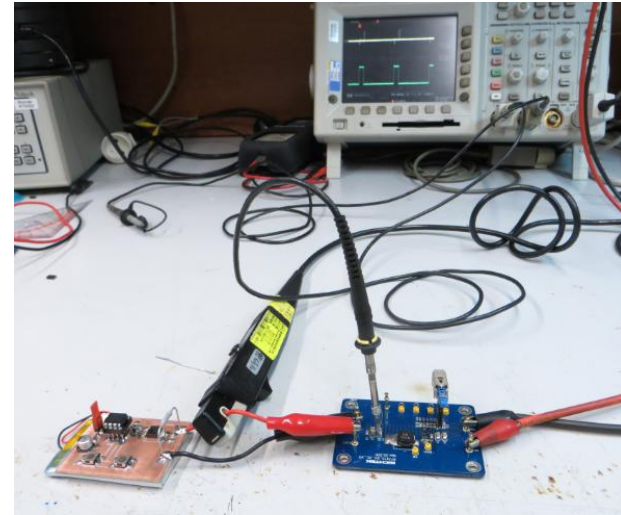


ACOT FAQ: Calculate and measure **output sag** during load transient

Measurement method:

Apply a fast step load 1~2A/μsec at converter output, using dynamic load or MOSFET switch (or use a power resistor briefly touching the load)

Measurement setup:



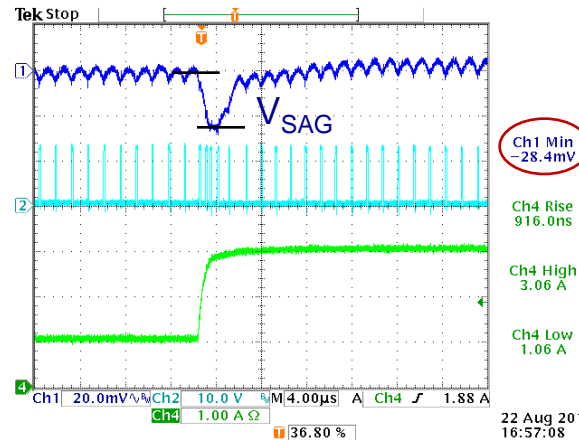
Output voltage sag happens during load transient rising edge

Calculation method:

$$V_{SAG} = \frac{L \times (\Delta I_{OUT})^2}{2 \times C_{OUT} \times (V_{IN} \times D_{MAX} - V_{OUT})}$$

$$t_{ON} = \frac{V_{OUT}}{V_{IN} \times f_{SW}} \text{ and } D_{MAX} = \frac{t_{ON}}{t_{ON} + t_{OFF(MIN)}}$$

Measurement result:



(measured V_{SAG} is lower than calculated due to rise time of load step)

In RT7275GQW 1.05V demo board and 2A fast load step:

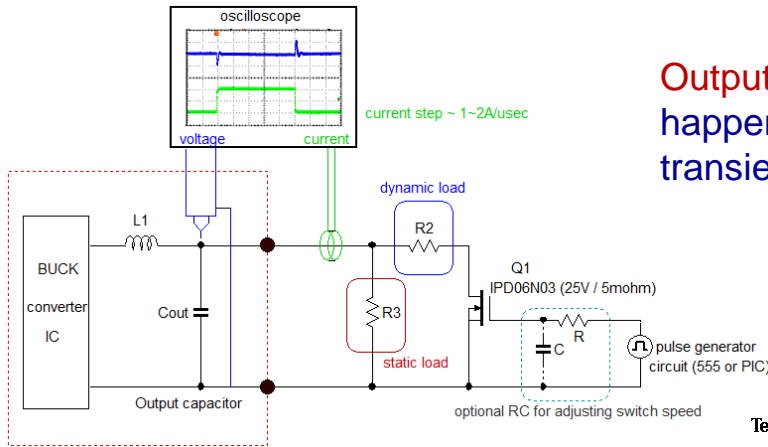
$$V_{SAG} = \frac{1.4\mu H \cdot 2A^2}{2 \cdot 22\mu F \cdot (12 \cdot 0.35 - 1.05)} = 40mV$$

22 Aug 2014 16:57:08

ACOT FAQ: Calculate and measure **output soar** during load transient

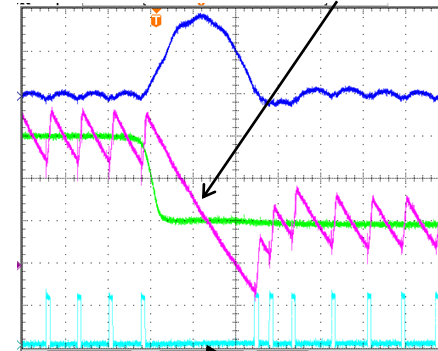
Measurement method:

Apply a fast step load $1\sim 2A/\mu\text{sec}$ at converter output, using dynamic load or MOSFET switch (or use a power resistor briefly touching the load)



Output voltage soar happens during load transient **falling edge**

The inductor current drops slower than load current, thereby charging the output capacitor



Converter in 0% duty-cycle to maximize output discharge

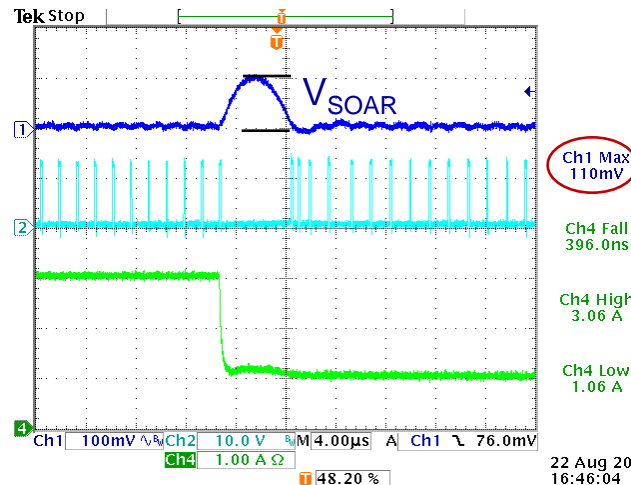
Calculation method:

$$V_{SOAR} = \frac{L \times (\Delta I_{OUT})^2}{2 \times C_{OUT} \times V_{OUT}}$$

In 1.05V demo board and 2A fast load step:

$$V_{SOAR} = \frac{1.4\mu H \cdot 2A^2}{2 \cdot 22\mu F \cdot 1.05V} = 121mV$$

Measurement result:

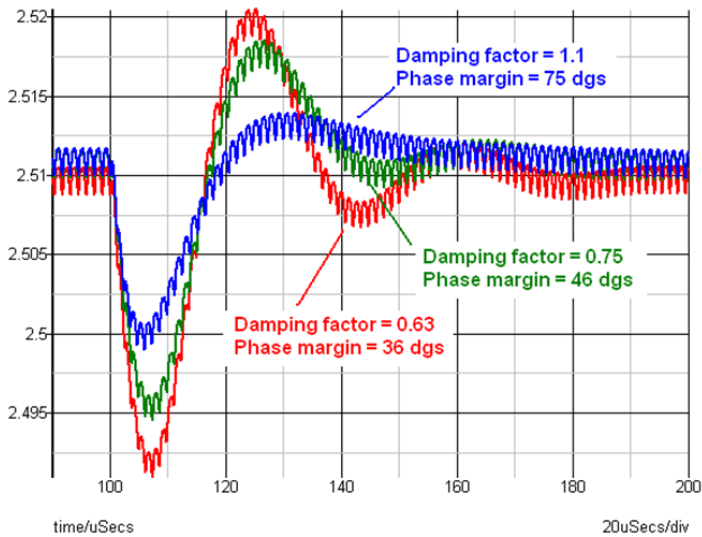


Measured V_{SOAR} is lower than calculated due to fall time of load step

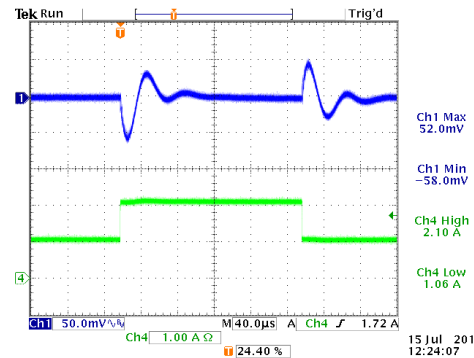
(soar pulse may have different amplitude depending on timing of load step relative to the last switching on-time)

ACOT FAQ: How to check converter stability

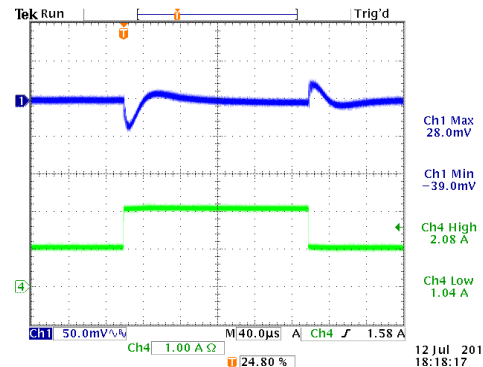
ACOT uses a non-linear constant ON time control system, and traditional open loop gain-phase stability analysis methods are not suitable to be used with ACOT converters. *Closed loop* analysis is valid for ACOT and can be used for mathematical calculations. For practical stability measurements, it is recommended to use **fast step loads** to measure the converter damping. Sufficiently damped response **will not show any ringing**, and corresponds to a stable control loop.



Relation between step load response ringing, damping and phase margin

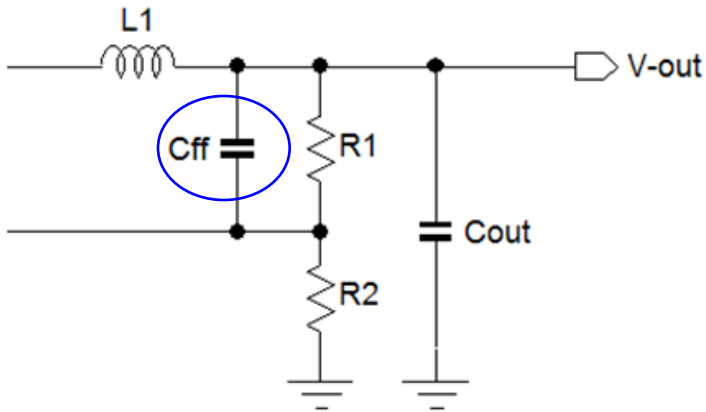


Step load measurement showing under-damped response (Cff needs to be added or increased in value)



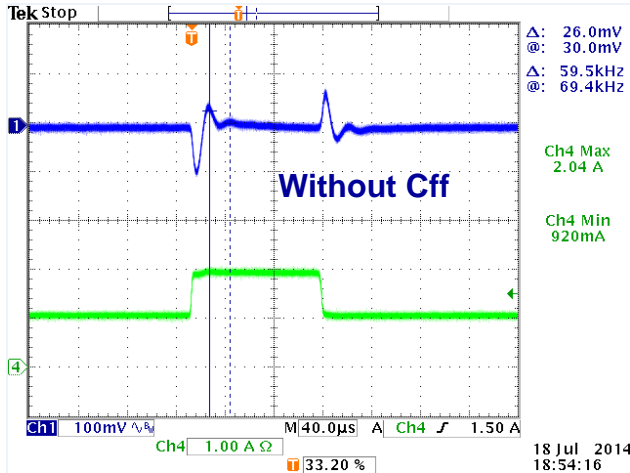
Step load measurement showing well-damped response

ACOT FAQ: How to tune Cff



The feed-forward capacitor plays a role in the damping of the ACOT control loop, especially at high duty-cycle applications like 12V → 5V. For low duty-cycle applications like 12V → 1V it is normally not needed. The value of C_{ff} for a specific ACOT converter depends on duty-cycle, C_{OUT} value, inductor value and R1 value.

Practical method to find Cff value:

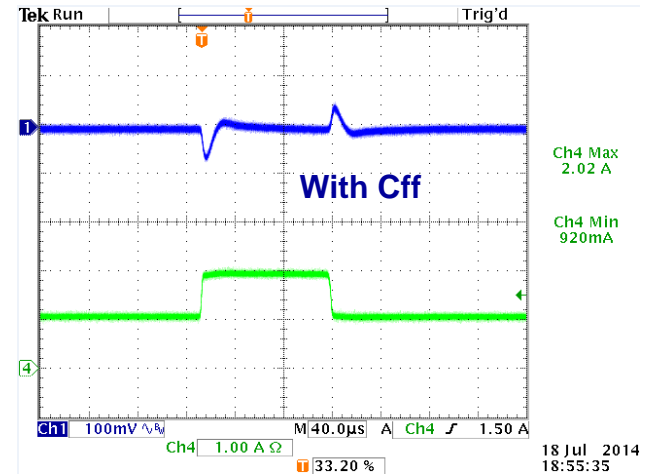


2. Calculate C_{FF} by the formula:

$$C_{FF} = \frac{1}{2\pi \cdot R1 \cdot f_{RING} \cdot 0.8}$$

In this example: (R1 = 120k)

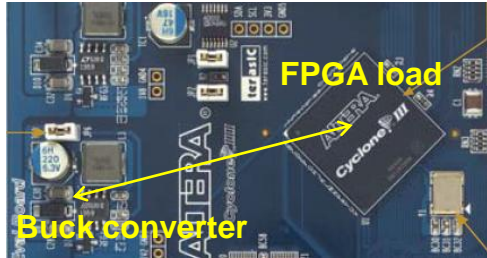
$$\frac{1}{2\pi \cdot 120k \cdot 59.5k \cdot 0.8} = 27.9pF$$



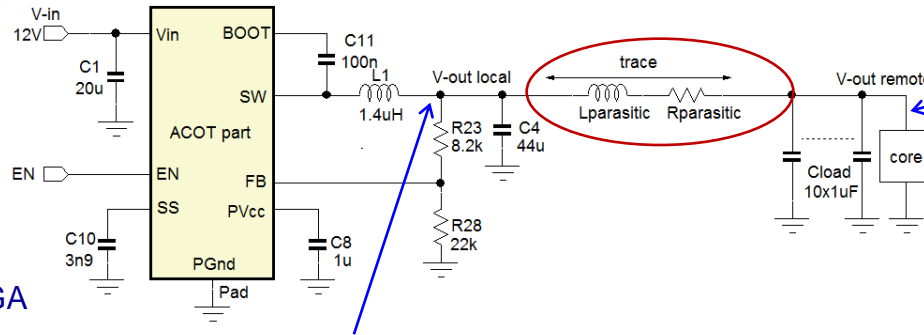
1. Apply a step load and if it shows ringing, measure the ringing frequency
 In this 12V → 5V example: f_{RING}=59.5kHz

After adding C_{ff} = 27pF: well-damped step response

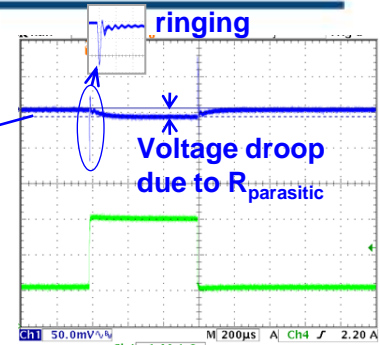
ACOT FAQ: ACOT converter with remote sense



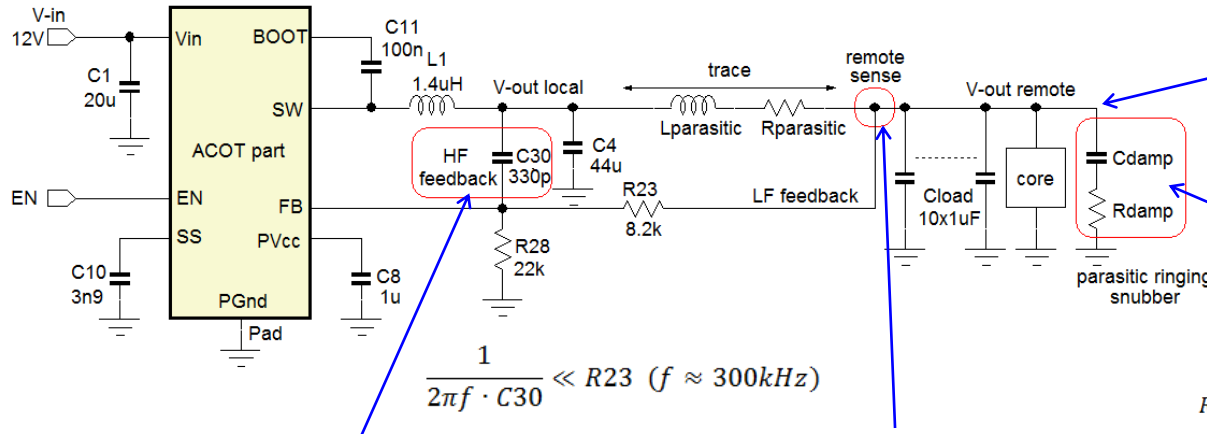
Distance between converter and FPGA



Converter regulates V_{OUT} local



Solution: Use remote sense



$$\frac{1}{2\pi f \cdot C30} \ll R23 \quad (f \approx 300kHz)$$

Add RC snubber at load side to damp the ringing that can happen due to $L_{PARASITIC}$ and C_{LOAD}

$$R_{SNUBBER} = \sqrt{\frac{L_{PARASITIC}}{C_{LOAD}}} \approx \sqrt{\frac{30nH}{10\mu F}} = 55m\Omega$$

$$C_{SNUBBER} > \frac{2\pi\sqrt{L_{PARASITIC} \cdot C_{LOAD}}}{R_{SNUBBER}} \approx \frac{2\pi\sqrt{30nH \cdot 10\mu F}}{55m\Omega} = 62\mu F$$

(you can use OSCON capacitor as snubber)

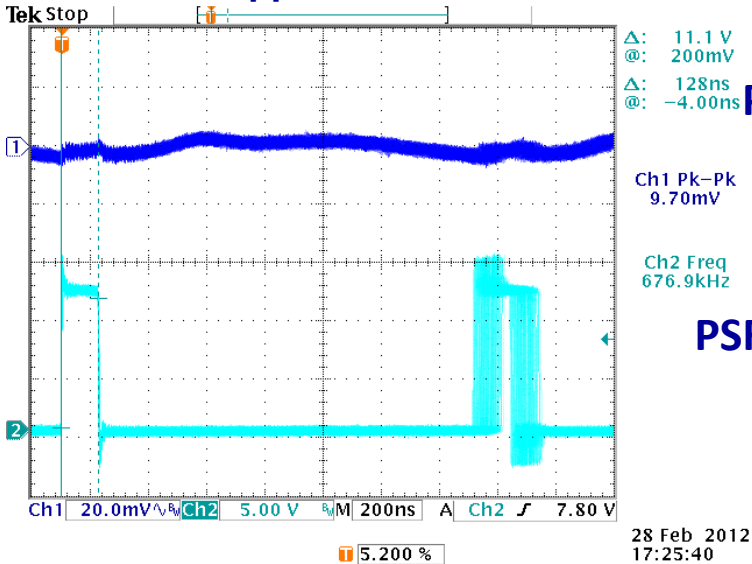
Use capacitor from V_{OUT} local to feedback to avoid instability due to $L_{PARASITIC}$ & C_{OUT} phase delay

Feedback resistor connection at remote load side

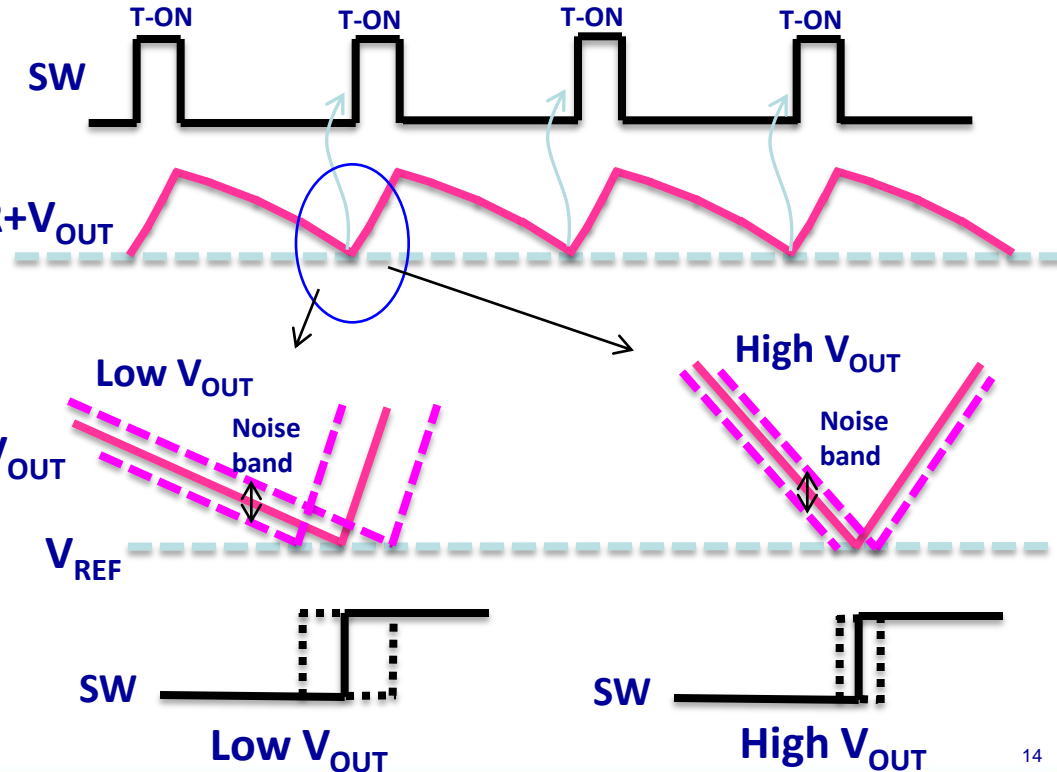
ACOT FAQ: Why do switch waveforms show frequency jitter?

ACOT uses a (pseudo) fixed T_{ON} , and controls T_{OFF} to regulate the output voltage. This means that load transients will always result in frequency changes in the switch waveform. At steady load conditions, the duty-cycle will be constant, and the frequency locked loop will slowly control T_{ON} for operation near the nominal frequency. However, there will always be some frequency jitter visible in the switch waveform due to noise in the feedback signal. At low V_{OUT} applications, frequency jitter will be more than at high V_{OUT} applications.

V_{OUT} and switching waveform for a 12V → 1.0V application



Switching waveform shows ~ 7% jitter

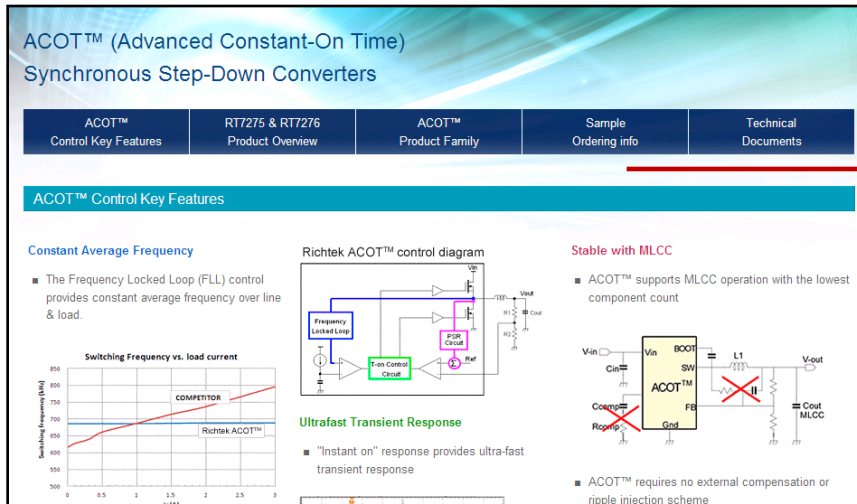


□ ACOT™ Design tools & Application notes

Richtek Website ACOT™ Landing Pages



Click ACOT banner or search for "ACOT"



ACOT Landing page with more info on specific products

ACOT™ Video

ACOT™ video Youtube

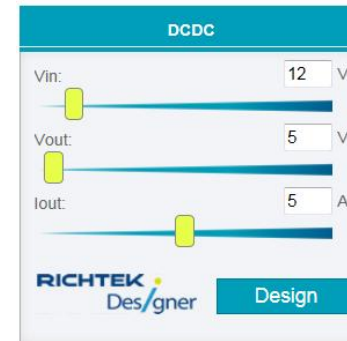


ACOT™ video Tudou: ENGLISH CHINESE

ACOT™ video YouKu: ENGLISH CHINESE

Application notes, design tools and tutorial videos

Design Tool NEW!



Application Note

- NEW! SOT-23 FCOL Thermal Considerations
- NEW! ACOT™ Stability Testing

Richtek Website Product Pages

Application notes and tools can be found under "Documents and Tools" tab

RT7275/RT7276

3A, 18V, 700kHz ACOT™ Synchronous Step-Down Converter


Datasheet 

Overview


Documents & Tools

Ordering Information

Datasheets

| Title | Description | Size | Last Updated |
|--|------------------------------|--------|--------------|
|  DS7275_76-00.pdf | Datasheets for RT7275/RT7276 | 359 KB | 2014 Jul |

Application Notes

| Download | Title | Last Updated |
|--|---|--------------|
|  | ACOT™ Stability Testing | 2013-11-07 |

Design Tool

| Type | Title |
|---|---|
|  | Richtek Designer™ Web Simulation Tool |

RICHTEK
your power partner.

thank you.