## 2A, 1MHz, 6V CMCOT Synchronous Step-Down Converter

### **General Description**

The RT5712C is a high efficiency synchronous step-down DC-DC converter. Its input voltage range is from 2.7V to 6V and provides an adjustable regulated output voltage from 0.6V to 3.4V while delivering up to 2A of output current.

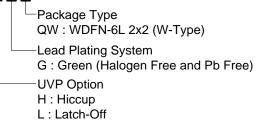
The internal synchronous low on-resistance power switches increase efficiency and eliminate the need for an external Schottky diode. The Current Mode Constant-On-time (CMCOT) operation with internal compensation allows the transient response to be optimized over a wide range of loads and output capacitors.

### Applications

- STB, Cable Modem, & xDSL Platforms
- LCD TV Power Supply & Metering Platforms
- General Purpose Point of Load (POL)

### **Ordering Information**

### RT5712C

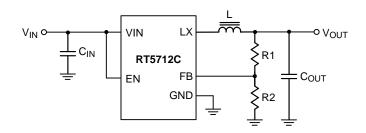


#### Note :

Richtek products are :

- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ▶ Suitable for use in SnPb or Pb-free soldering processes.

## **Simplified Application Circuit**

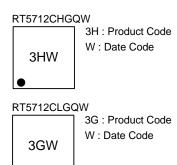


#### Copyright © 2021 Richtek Technology Corporation. All rights reserved. RICHTEK is a registered trademark of Richtek Technology Corporation. DS5712C-05

### **Features**

- Efficiency Up to 95%
- R<sub>DSON</sub> 100mΩ HS / 70mΩ LS
- V<sub>IN</sub> Range 2.7V to 6V
- V<sub>REF</sub> 0.6V with ±1.5% Accuracy
- CMCOT<sup>™</sup> Control Loop Design for Best Transient Response, Robust Loop Stability with Low-ESR (MLCC) COUT
- Fixed Soft-Start 1.2ms
- Cycle-by-Cycle Over-Current Protection
- Input Under-Voltage Lockout
- Output Under-Voltage Protection (UVP Hiccup)
- Thermal Shutdown Protection
- Power Saving at Light Load

## Marking Information



## Pin Configuration

(TOP VIEW)					
NC	1	GND	6	FB	
EN	2		5	GND	
VIN	3		4	LX	

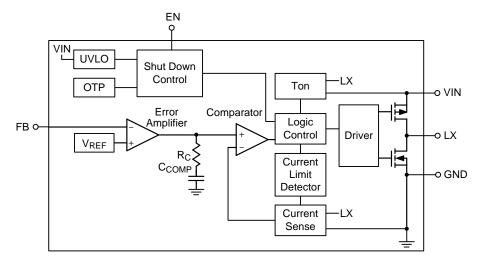
WDFN-6L 2x2



### **Functional Pin Description**

Pin No.	Pin Name	Pin Function		
1	NC	No internal connection.		
2	EN	Enable control input.		
3	VIN	Supply voltage input. The RT5712C operates from a 2.7V to 6V input.		
4	LX	Switch node.		
5, 7 (Exposed Pad)	GND	Ground. The exposed pad must be soldered to a large PCB and connected to GND for maximum thermal dissipation.		
6	FB	Feedback.		

### **Functional Block Diagram**



## Operation

The RT5712C is a synchronous low voltage step-down converter that can support the input voltage range from 2.7V to 6V and the output current can be up to 2A. The RT5712C uses a constant on-time, current mode architecture. In normal operation, the high side P-MOSFET is turned on when the switch controller is set by the comparator and is turned off when the Ton comparator resets the switch controller.

Low side MOSFET peak current is measured by internal RSENSE. The error amplifier EA adjusts COMP voltage by comparing the feedback signal (V<sub>FB</sub>) from the output voltage with the internal 0.6V reference. When the load current increases, it causes a drop in the feedback voltage relative to the reference, then the COMP voltage rises to allow higher inductor current to match the load current.

### **UV** Comparator

If the feedback voltage ( $V_{FB}$ ) is lower than threshold voltage 0.2V, the UV comparator's output will go high and the switch controller will turn off the high side MOSFET. The output under voltage protection is designed to operate in Hiccup and Latch-off mode.

### **Enable Comparator**

A logic-high enables the converter; a logic-low forces the IC into shutdown mode.

### Soft-Start (SS)

An internal current source charges an internal capacitor to build the soft-start ramp voltage. The  $V_{FB}$  voltage will track the internal ramp voltage during soft-start interval. The typical soft-start time is 1.2ms.

### **Over-Current Protection (OCP)**

The RT5712C provides over-current protection by detecting low side MOSFET valley inductor current. If the sensed valley inductor current is over the current limit threshold (2.9A typ.), the OCP will be triggered. When OCP is tripped, the RT5712C will keep the over current threshold level until the over current condition is removed.

### **Thermal Shutdown (OTP)**

The device implements an internal thermal shutdown function when the junction temperature exceeds 150°C. The thermal shutdown forces the device to stop switching when the junction temperature exceeds the thermal shutdown threshold. Once the die temperature decreases below the hysteresis of 20°C, the device reinstates the power up sequence.

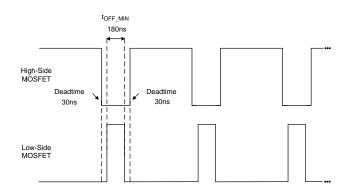
### Maximum Duty Cycle

The maximum duty cycle (70%, min.) can be calculated by minimum off time (180ns, max.), dead time (60ns, max.) and switching frequency (1.2MHz, max.).

 $D_{MAX} = 1 - (t_{OFF}MIN + t_D) x f_{SW}$ 

Where  $t_{OFF\_MIN}$  is minimum off time,  $t_D$  is dead time and  $f_{SW}$  is switching frequency.

If input voltage and output voltage are closed, RT5712C operates at high duty cycle. Once the operational duty cycle is larger than the maximum duty cycle (70%, min.), RT5712C keeps minimum off time (180ns, max.) and deadtime (60ns, max.), then the output voltage starts to drop. The input voltage at which the devices enter dropout changes depending on the input voltage, output voltage, switching frequency, load current, and the efficiency of the design.





## Absolute Maximum Ratings (Note 1)

Supply Input Voltage	–0.3V to 6.5V
LX Pin Switch Voltage	–0.3V to (V <sub>IN</sub> + 0.3V)
<20ns	-4.5V to 7.5V
<ul> <li>Power Dissipation, PD @ T<sub>A</sub> = 25°C</li> </ul>	
WDFN-6L 2x2	0.833W
Package Thermal Resistance (Note 2)	
WDFN-6L 2x2, θ <sub>JA</sub>	120°C/W
WDFN-6L 2x2, θ <sub>JC</sub>	7°C/W
Lead Temperature (Soldering, 10 sec.)	260°C
Junction Temperature	–40°C to 150°C
Storage Temperature Range	–65°C to 150°C
ESD Susceptibility (Note 3)	
HBM (Human Body Model)	2kV

### Recommended Operating Conditions (Note 4)

•	Supply Input Voltage	2.7V to 6V
•	Ambient Temperature Range	–40°C to 85°C
•	Junction Temperature Range	–40°C to 125°C

## **Electrical Characteristics**

$(V_{IN} = 3.6V, T_A = 25^{\circ}C, unless otherwise specific$	ed)
--	-----

Parameter		Symbol	Test Conditions	Min	Тур	Max	Unit	
Input Voltage		VIN		2.7		6	V	
Feedback Refere	ence Voltage	V <sub>REF</sub>		0.591	0.6	0.609	V	
Feedback Leaka	ge Current	I <sub>FB</sub>	V <sub>FB</sub> = 0.6V			0.1	μA	
DC Bias Current			Active, $V_{FB} = 0.63V$ , not switching		22			
			Shutdown			1	μA	
Switching Leaka	ge Current					1	μA	
Switching Frequency					1		MHz	
Switch On Resistance, High		R <sub>PMOS</sub>	I <sub>SW</sub> = 0.3A		100		mΩ	
Switch On Resistance, Low		R <sub>NMOS</sub>	Isw = 0.3A		70		mΩ	
Valley Current Limit		I <sub>LIM</sub>		2.1	2.9	3.8	А	
Under-Voltage Lo	ockout	N/	VDD rising		2.25	2.5		
Threshold		VUVLO	VDD falling		2		V	
Over-Temperature Threshold					150		°C	
Enable Input Logic-High		Vih		1.2			V	
Voltage	Logic-Low	VIL				0.4	v	
Soft-Start Time		T <sub>SS</sub>			1.2		ms	

## **RT5712C**

Parameter	Symbol	Test Conditions	Min	Тур	Мах	Unit
Minimum Off Time				120		ns
Maximum Duty Cycle	DMAX	(Note 5)	70			%
Output Discharge Switch On Resistance				1.8		kΩ

**Note 1.** Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.

Note 2.  $\theta_{JA}$  is measured at  $T_A = 25^{\circ}C$  on a high effective thermal conductivity four-layer test board per JEDEC 51-7.  $\theta_{JC}$  is measured at the exposed pad of the package.

Note 3. Devices are ESD sensitive. Handling precaution recommended.

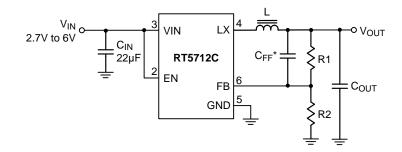
Note 4. The device is not guaranteed to function outside its operating conditions.

Note 5. Guaranteed by design.





## **Typical Application Circuit**

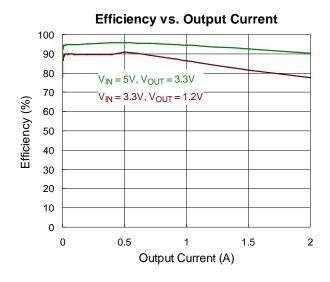


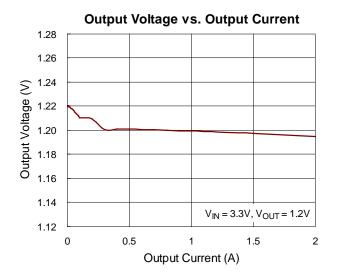
\*CFF : Optional for performance fine-tune

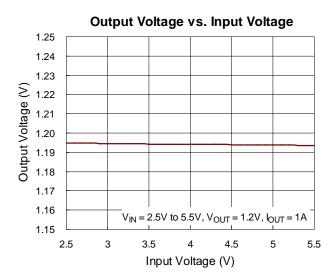
V <sub>OUT</sub> (V)	<b>R1 (k</b> Ω)	<b>R2 (k</b> Ω)	<b>L (</b> μ <b>H)</b>	<b>C<sub>OUT</sub> (μF)</b>
3.3	90	20	1 to 3.3	22
1.8	100	50	1 to 3.3	22
1.5	100	66.6	1 to 3.3	22
1.2	100	100	1 to 3.3	22
1.05	100	133	1 to 3.3	22
1	100	148	1 to 3.3	22

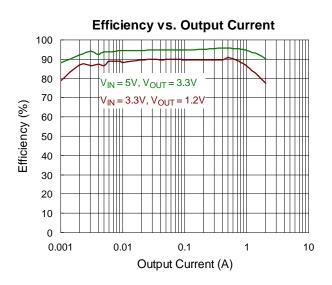
## **Typical Operating Characteristics**

RICHTEK

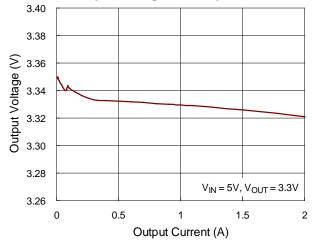


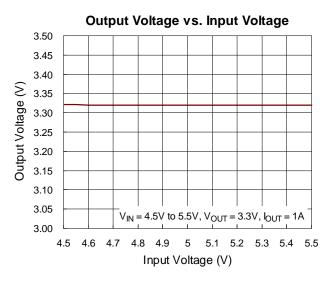






**Output Voltage vs. Output Current** 





Copyright © 2021 Richtek Technology Corporation. All rights reserved. RICHTEK is a registered trademark of Richtek Technology Corporation. DS5712C-05 June 2021

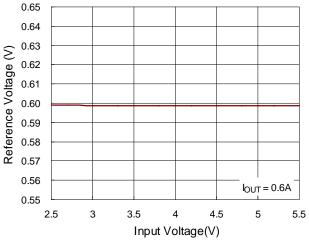
www.richtek.com

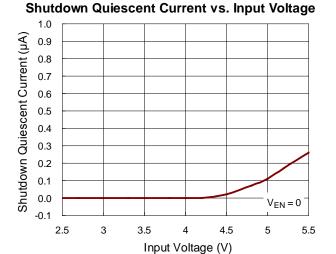
7

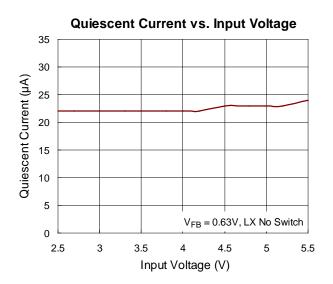


RICHTEK

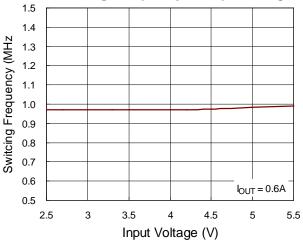
Reference Voltage vs Input Voltage



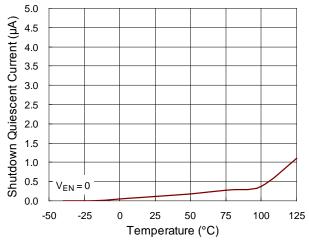


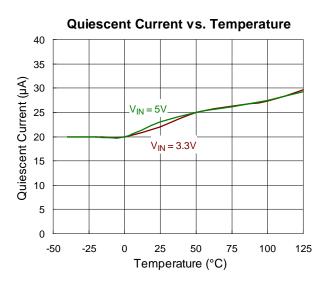


Switching Frequency vs. Input Voltage

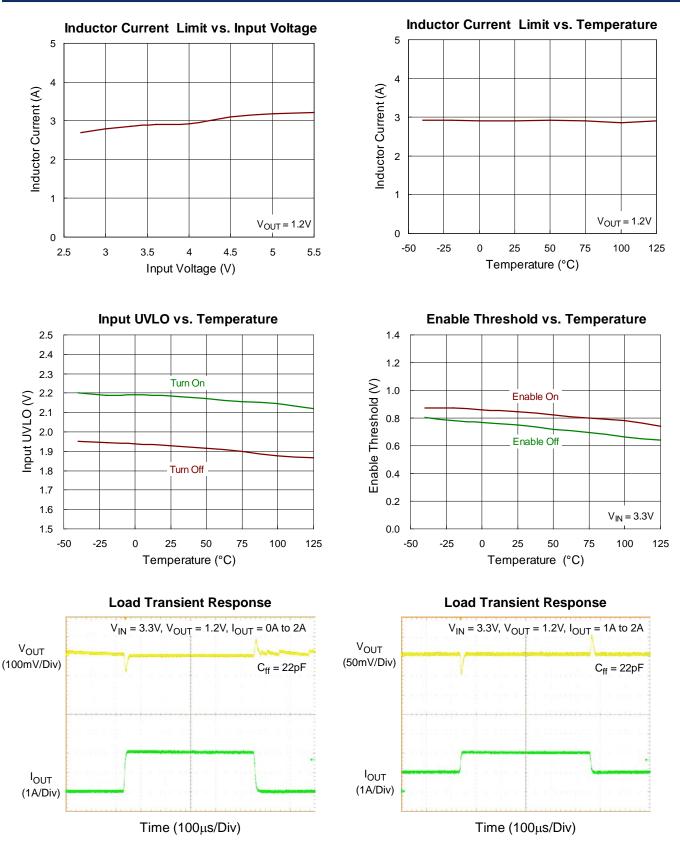


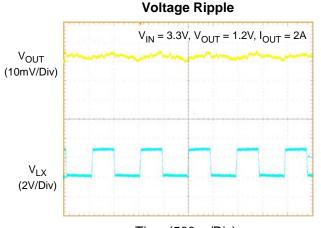
Shutdown Quiescent Current vs. Temperature



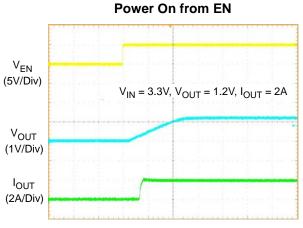


Copyright © 2021 Richtek Technology Corporation. All rights reserved. RICHTEK is a registered trademark of Richtek Technology Corporation.

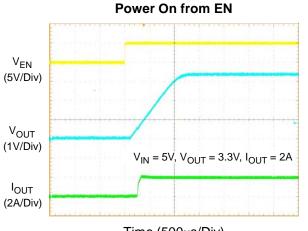




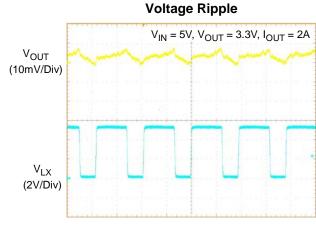
Time (500ns/Div)



Time (500µs/Div)



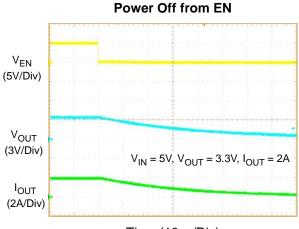
Time (500µs/Div)



Time (500ns/Div)



Time (10µs/Div)



Time (10µs/Div)

Power Off from EN



### **Application Information**

The RT5712C is a single-phase step-down converter. It provides single feedback loop, constant on-time current mode control with fast transient response. An internal 0.6V reference allows the output voltage to be precisely regulated for low output voltage applications. A fixed switching frequency (1MHz) oscillator and internal compensation are integrated to minimize external component count. Protection features include over-current protection, under-voltage protection and over-temperature protection.

### **Output Voltage Setting**

Connect a resistive voltage divider at the FB between VOUT and GND to adjust the output voltage. The output voltage is set according to the following equation :

$$V_{OUT} = V_{REF} \times \left(1 + \frac{R1}{R2}\right)$$

where VREF is the feedback reference voltage 0.6V (typ.).

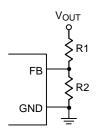


Figure 1. Setting VOUT with a Voltage Divider

#### **Chip Enable and Disable**

The EN pin allows for power sequencing between the controller bias voltage and another voltage rail. The RT5712C remains in shutdown if the EN pin is lower than 400mV. When the EN pin rises above the VEN trip point, the RT5712C begins a new initialization and soft-start cycle.

#### **Internal Soft-Start**

The RT5712C provides an internal soft-start function to prevent large inrush current and output voltage overshoot when the converter starts up. The soft-start (SS) automatically begins once the chip is enabled. During soft-start, the internal soft-start capacitor becomes charged and generates a linear ramping up voltage across the capacitor. This voltage clamps the voltage at the FB pin, causing PWM pulse width to increase slowly and in turn reduce the input surge current. The internal 0.6V reference takes over the loop control once the internal ramping-up voltage becomes higher than 0.6V.

#### **Over-Voltage Protection (OVP)**

The RT5712CL provide Over-Voltage Protection function when output voltage over 120%. The IC will be into Latch-off mode.

### **UVLO Protection**

The RT5712C has input Under Voltage Lockout protection (UVLO). If the input voltage exceeds the UVLO rising threshold voltage (2.25V typ.), the converter resets and prepares the PWM for operation. If the input voltage falls below the UVLO falling threshold voltage during normal operation, the device will stop switching. The UVLO rising and falling threshold voltage has a hysteresis to prevent noise-caused reset.

### **Inductor Selection**

The switching frequency (on-time) and operating point (% ripple or LIR) determine the inductor value as shown below :

$$L = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{f_{SW} \times LIR \times I_{LOAD(MAX)} \times V_{IN}}$$

where LIR is the ratio of the peak-to-peak ripple current to the average inductor current.

Find a low loss inductor having the lowest possible DC resistance that fits in the allotted dimensions. The core must be large enough not to saturate at the peak inductor current (IPEAK) :

$$I_{PEAK} = I_{LOAD(MAX)} + \left(\frac{LIR}{2} \times I_{LOAD(MAX)}\right)$$

The calculation above serves as a general reference. To further improve transient response, the output inductor can be further reduced. This relation should be considered along with the selection of the output capacitor.

Inductor saturation current should be chosen over IC's current limit.

#### **Input Capacitor Selection**

High quality ceramic input decoupling capacitor, such as X5R or X7R, with values greater than  $10\mu F$  are recommended for the input capacitor. The X5R and

X7R ceramic capacitors are usually selected for power regulator capacitors because the dielectric material has less capacitance variation and more temperature stability.

Voltage rating and current rating are the key parameters when selecting an input capacitor. Generally, selecting an input capacitor with voltage rating 1.5 times greater than the maximum input voltage is a conservatively safe design.

The input capacitor is used to supply the input RMS current, which can be approximately calculated using the following equation :

$$I_{IN\_RMS} = I_{LOAD} \times \sqrt{\frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)}$$

The next step is selecting a proper capacitor for RMS current rating. One good design uses more than one capacitor with low equivalent series resistance (ESR) in parallel to form a capacitor bank.

The input capacitance value determines the input ripple voltage of the regulator. The input voltage ripple can be approximately calculated using the following equation :

$$\Delta V_{\text{IN}} = \frac{I_{\text{OUT}}(\text{MAX})}{C_{\text{IN}} \times f_{\text{SW}}} \times \frac{V_{\text{OUT}}}{V_{\text{IN}}} \times \left(1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}\right)$$

#### **Output Capacitor Selection**

The output capacitor and the inductor form a low pass filter in the Buck topology. In steady state condition, the ripple current flowing into/out of the capacitor results in ripple voltage. The output voltage ripple (VP-P) can be calculated by the following equation :

$$V_{P\_P} = LIR \times I_{LOAD(MAX)} \times \left(ESR + \frac{1}{8 \times C_{OUT} \times f_{SW}}\right)$$

When load transient occurs, the output capacitor supplies the load current before the controller can respond. Therefore, the ESR will dominate the output voltage sag during load transient. The output voltage undershoot ( $V_{SAG}$ ) can be calculated by the following equation :

For a given output voltage sag specification, the ESR value can be determined.

Another parameter that has influence on the output voltage sag is the equivalent series inductance (ESL). The rapid change in load current results in di/dt during transient. Therefore, the ESL contributes to part of the voltage sag. Using a capacitor with low ESL can obtain better transient performance. Generally, using several capacitors connected in parallel can have better transient performance than using a single capacitor for the same total ESR.

#### **Thermal Considerations**

For continuous operation, do not exceed absolute maximum junction temperature. The maximum power dissipation depends on the thermal resistance of the IC package, PCB layout, rate of surrounding airflow, and difference between junction and ambient temperature. The maximum power dissipation can be calculated by the following formula :

#### $\mathsf{P}_{\mathsf{D}(\mathsf{MAX})} = (\mathsf{T}_{\mathsf{J}(\mathsf{MAX})} - \mathsf{T}_{\mathsf{A}}) / \theta_{\mathsf{J}\mathsf{A}}$

where  $T_{J(MAX)}$  is the maximum junction temperature,  $T_A$  is the ambient temperature, and  $\theta_{JA}$  is the junction to ambient thermal resistance.

For recommended operating condition specifications, the maximum junction temperature is 125°C. The junction to ambient thermal resistance,  $\theta_{JA}$ , is layout dependent. For WDFN-6L 2x2 package, the thermal resistance,  $\theta_{JA}$ , is 120°C/W on a standard four-layer thermal test board. The maximum power dissipation at  $T_A = 25^{\circ}$ C can be calculated by the following formula :

 $P_{D(MAX)} = (125^{\circ}C - 25^{\circ}C) / (120^{\circ}C/W) = 0.833W$  for WDFN-6L 2x2 package

The maximum power dissipation depends on the operating ambient temperature for fixed  $T_{J(MAX)}$  and thermal resistance,  $\theta_{JA}$ . The derating curve in Figure 2 allows the designer to see the effect of rising ambient temperature on the maximum power dissipation.

 $V_{SAG} = \Delta I_{LOAD} \times ESR$ 

Copyright © 2021 Richtek Technology Corporation. All rights reserved.
 RICHTEK is a registered trademark of Richtek Technology Corporation.

 www.richtek.com
 DS5712C-05
 June
 2021



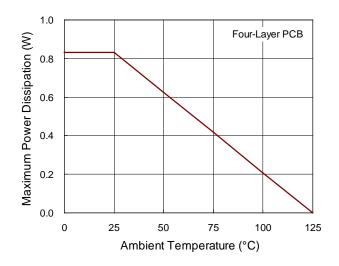
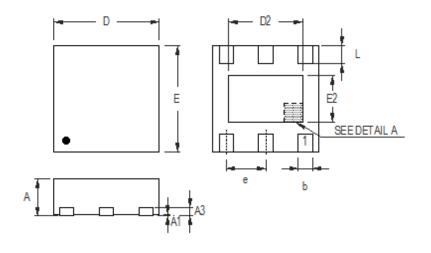
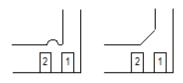


Figure 2. Derating Curve of Maximum Power Dissipation

## **Outline Dimension**





DETAIL A Pin #1 ID and Tie Bar Mark Options

Note : The configuration of the Pin #1 identifier is optional, but must be located within the zone indicated.

Symbol	Dimensions	In Millimeters	<b>Dimensions In Inches</b>		
	Min	Max	Min	Max	
А	0.700	0.800	0.028	0.031	
A1	0.000	0.050	0.000	0.002	
A3	0.175	0.250	0.007	0.010	
b	0.200	0.350	0.008	0.014	
D	1.950	2.050	0.077	0.081	
D2	1.000	1.450	0.039	0.057	
E	1.950	2.050	0.077	0.081	
E2	0.500	0.850	0.020	0.033	
е	0.650		0.0	)26	
L	0.300	0.400	0.012	0.016	

W-Type 6L DFN 2x2 Package

### **Richtek Technology Corporation** 14F, No. 8, Tai Yuen 1<sup>st</sup> Street, Chupei City

14F, No. 8, Tai Yuen 1<sup>st</sup> Street, Chupei City Hsinchu, Taiwan, R.O.C. Tel: (8863)5526789

Richtek products are sold by description only. Richtek reserves the right to change the circuitry and/or specifications without notice at any time. Customers should obtain the latest relevant information and data sheets before placing orders and should verify that such information is current and complete. Richtek cannot assume responsibility for use of any circuitry other than circuitry entirely embodied in a Richtek product. Information furnished by Richtek is believed to be accurate and reliable. However, no responsibility is assumed by Richtek or its subsidiaries for its use; nor for any infringements of patents or other rights of third parties which may result from its use. No license is granted by implication or otherwise under any patent or patent rights of Richtek or its subsidiaries.

Copyright © 2021 Richtek Technology Corporation. All rights reserved. RICHTEK is a registered trademark of Richtek Technology Corporation.

www.richtek.com